

Optimal management of energy resources in greenhouse crop production systems

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Background



- Greenhouse horticulture is a large consumer of fossil energy.
- Growers have to reduce energy consumption and CO₂ emission
- Growers have installed a wide range of auxiliary equipment to produce, consume and store energy.
 - Increased complexity and interconnectivity of the various resources.
 - Complex management task.

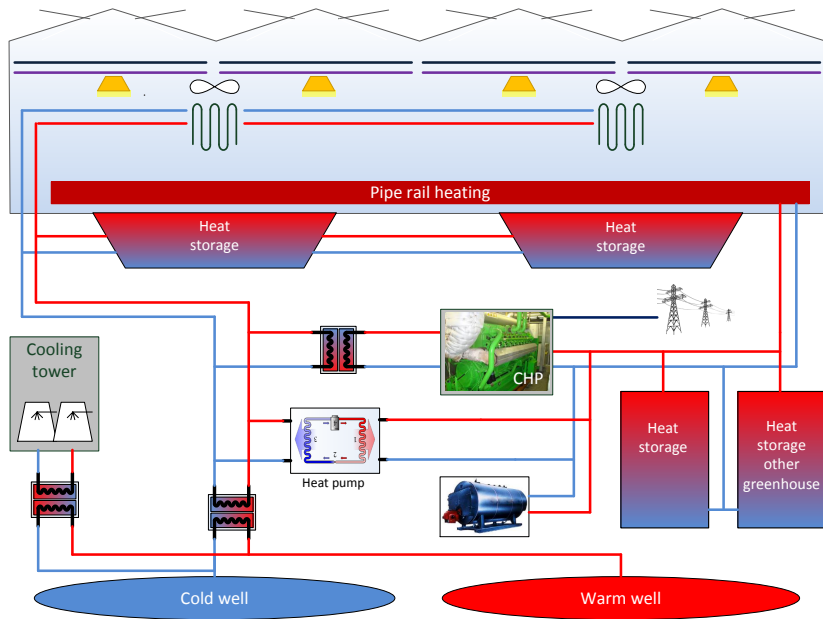
Optimal management of energy resources

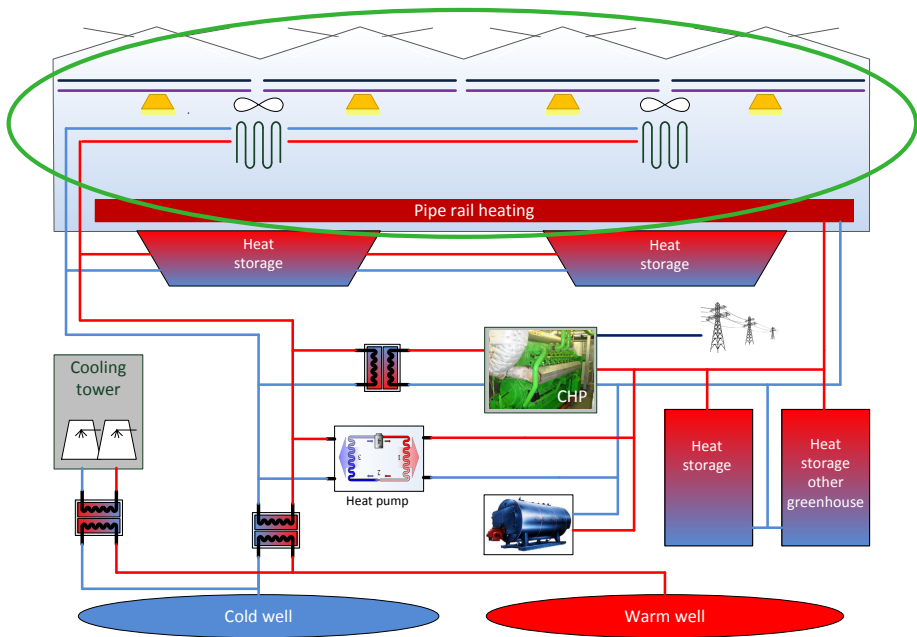
Goal:

Utilize all equipment in a modern greenhouse in the most efficient manner.



Figure : 4 ha commercial rose greenhouse





Dual-stage approach

Stage 1: Create a desired climate in the greenhouse with minimal energy input.

Stage 2: Generate this energy as efficient as possible with the available equipment.



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Why?

- OCAP CO₂ is used
- Buffer capacity available
- Practical reasons

Stage 1: Create a desired climate using minimal energy

What is the desired climate?

- Grower knows best about the crop
- Ideal climate depends on
 - weather predictions
 - status of the crop
 - specific crop knowledge
 - production prognosis
 - product price prognosis
 - experience of the grower
 - ...



The desired climate

1. Let the grower define bounds to specify the desired climate
 - Upper and lower bounds for temperature
 - Upper bound for humidity
 - Upper and lower bounds for CO₂
 - Maximum amount of CO₂ available per day

Advantages

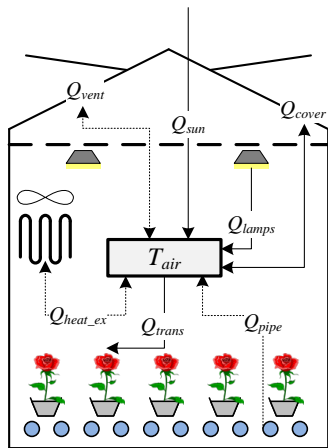
- No crop production models needed
- No predictions of market prices needed

2. Minimize total energy input by using optimal control techniques
 - Model of greenhouse climate is needed.

The dynamic model (1)

Energy balance

$$\frac{dT_{air}}{dt} = \frac{1}{C_{cap}} (Q_{sun} - Q_{cover} - Q_{trans} + Q_{lamps} - Q_{vent} + Q_{he} + Q_{pipe}) \quad (^\circ\text{C s}^{-1})$$



Energy fluxes (W m^{-2}) (1)

- Q_{sun} = Radiation from sun
- Q_{cover} = Cover losses
- Q_{trans} = Crop transpiration
- Q_{lamps} = Artificial lighting
- Q_{vent} = Ventilation
- Q_{he} = OPAC heat exchanger
- Q_{pipe} = Pipe rail heating

See Van Beveren et al. (2013).

The dynamic model (2)

Humidity balance

$$\frac{d\chi_{air}}{dt} = \frac{1}{h} (\phi_{trans} - \phi_{cov} - \phi_{he} - \phi_{vent}) \quad (\text{g m}^{-3} \text{s}^{-1}) \quad (2)$$

CO₂ balance

$$\frac{dCO_{2_air}}{dt} = \frac{1}{h} (\phi_{c,inj} - \phi_{c,ass} - \phi_{c,vent}) \quad (\text{g m}^{-3} \text{s}^{-1}) \quad (3)$$

- See Van Beveren et al. (2015) for more details.
- The model is based on the work of Van Henten (1994), De Zwart (1996), Van Ooteghem (2007), and Vanthoor (2011).

External inputs of the model

■ Outdoor conditions

- Temperature ($^{\circ}\text{C}$)
- Relative Humidity (%)
- Radiation (W m^{-2})
- Wind speed (m s^{-1})
- CO_2 concentration (ppm)



■ Control inputs from the climate computer

- Screen closure (%)
- Artificial lighting (%)



Optimization procedure

- Optimal control formulation
- PROPT Matlab Optimal Control Software (Tomlab)

Optimal control problem (1)

Control variables:

1. Heating

- $Q_{E,heat} = Q_{he,heat} + Q_{pipe}$ in (W m^{-2})

2. Active cooling

- $Q_{E,cool} = Q_{he,cool}$ in (W m^{-2})

3. Ventilation

- $g_V =$ specific ventilation (m s^{-1})

4. CO₂ injection

- $\phi_{c,inj} =$ CO₂ injection flux ($\text{g m}^{-2} \text{s}^{-1}$).

Find control variables such that Eq. 4 is minimal.

$$\min_{Q_{E,heat}, Q_{E,cool}, g_V, \phi_{c,inj}} J = \int_{t_0}^{t_f} \left(Q_{E,heat}^2 + Q_{E,cool}^2 \right) dt \quad (4)$$

Optimal control problem (2) - Constraints

Climate variables

- Lower and upper temperature bound:

$$T_{air}^{min}(t) \leq T_{air}(t) \leq T_{air}^{max}(t) \quad (5)$$

- Upper bound for relative humidity:

$$RH_{air}(t) \leq RH_{air}^{max}(t) \quad (6)$$

- Lower and upper CO₂ bound:

$$CO_{2,air}^{min}(t) \leq CO_{2,air}(t) \leq CO_{2,air}^{max}(t) \quad (7)$$

Optimal control problem (2) - Constraints

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$$T_{air}^{min}(t) \leq T_{air}(t) \leq T_{air}^{max}(t) \quad (5)$$

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- Lower and upper CO₂ bound:

$$CO_{2,air}^{min}(t) \leq CO_{2,air}(t) \leq CO_{2,air}^{max}(t) \quad (7)$$

These are all set by the grower.

Optimal control problem (3) - Constraints

Control variables

- Heating capacity is limited by:

$$Q_{E,heat}^{min}(t) \leq Q_{E,heat}(t) \leq Q_{E,heat}^{max}(t) \quad (8)$$

- Cooling capacity is limited by:

$$Q_{E,cool}^{min}(t) \leq Q_{E,cool}(t) \leq Q_{E,cool}^{max}(t) \quad (9)$$

- Ventilation capacity is limited by:

$$g_V^{min}(t) \leq g_V(t) \leq g_V^{max}(t) \quad (10)$$

- CO₂ injection is limited by:

$$0 \leq \phi_{c,inj}(t) \leq \phi_{c,inj}^{max}(t) \quad (11)$$

- Total amount of CO₂ available per day is limited by:

$$\int_{t_0}^{t_f} \Phi_{c,inj} dt \leq \phi_{c,inj}^{max,day} \quad (12)$$

Optimal control problem (4) - Constraints

Dynamic greenhouse climate model

- Dynamic greenhouse climate model:

$$(\dot{T}_{air}, \dot{\chi}_{air}, \dot{CO}_{2,air}) = f(T_{air}, \chi_{air}, CO_{2,air}, Q_E, g_V, \phi_{c,inj}, t) \quad (13)$$

- Initial conditions:

$$T_{air}(t_0) = T_{air}(0), \chi_{air}(t_0) = \chi_{air}(0), CO_{2,air}(t_0) = CO_{2,air}(0) \quad (14)$$

Implementation of minimum pipe temperature

- Change lower bound for heating capacity

Minimum pipe temperature

Replace the old constraint

$$Q_{E,heat}^{min}(t) \leq Q_{E,heat}(t) \leq Q_{E,heat}^{max}(t) \quad (\text{W m}^{-2}) \quad (15)$$

with the new constraint with minimum pipe temperature T_{pipe}^{min} :

$$Q_{E,heat}^{min}(t) = \alpha_{pipe}(T_{pipe}^{min} - T_{air})(t) \quad (\text{W m}^{-2}) \quad (16)$$

- Similar approach for implementation of *minimum ventilation* is possible.

Standard optimization settings

Table : Standard settings of the bounds for optimization

| Symbol | Description | Value | Unit |
|--------------------------|---|--|---------------------------------|
| $T_{air}^{min}(t)$ | Lower temperature bound | $\bar{T}'_{air,meas}(t) - 0.5^{\circ}\text{C}$ | $^{\circ}\text{C}$ |
| $T_{air}^{max}(t)$ | Upper temperature bound | $\bar{T}'_{air,meas}(t) + 0.5^{\circ}\text{C}$ | $^{\circ}\text{C}$ |
| $RH_{air}^{max}(t)$ | Upper RH bound | $\max RH_{air,meas}(t)$ | % |
| $CO_{2,air}^{min}(t)$ | Lower CO ₂ bound | $0.97 \cdot \overline{CO}'_{2,air,meas}(t)$ | g m^{-3} |
| $CO_{2,air}^{max}(t)$ | Upper CO ₂ bound | 2000 ppm | g m^{-3} |
| $Q_{E,heat}^{max}(t)$ | Maximal heating capacity | 200 | W m^{-2} |
| $Q_{E,cool}^{min}(t)$ | Maximal cooling capacity | 200 | W m^{-2} |
| $\phi_{c,inj}^{max}(t)$ | Maximal CO ₂ injection capacity | 1200 | kg h^{-1} |
| $\Phi_{c,inj}^{max,day}$ | Total amount of CO ₂ available per day | $\int \phi_{c,inj,meas} dt$ | $\text{g m}^{-3} \text{d}^{-1}$ |

Table : Standard settings for optimization. ' = smoothed.

Optimization results

Optimization result 1 day

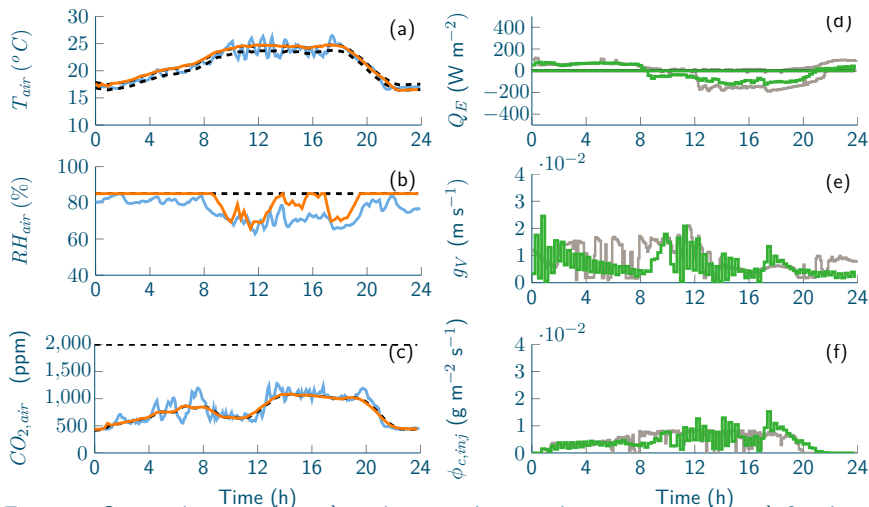


Figure : Optimal states (—) and optimal control trajectories (—) for June 16, 2012 with standard settings. The dashed lines are the bounds. The realized climate variables (—) and the control trajectories resulting from growers operation (—) are also shown.

One year optimization with standard settings

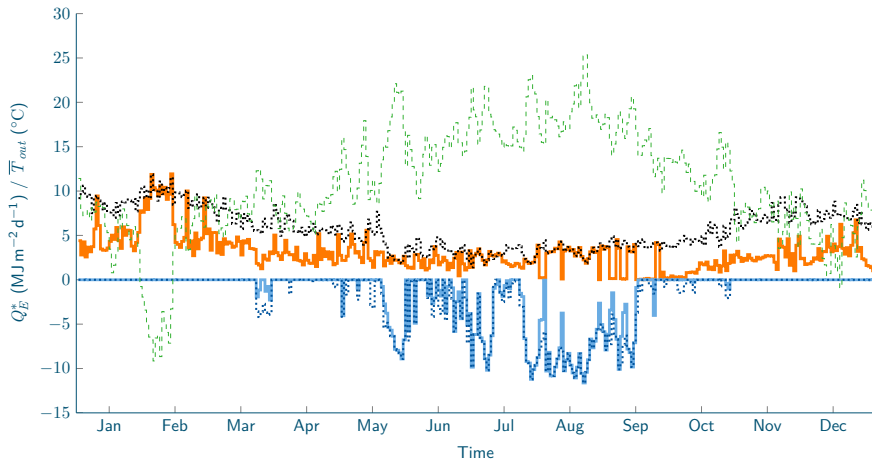


Figure : Results of daily optimization with standard settings for the year 2012. Optimal heating (—), optimal cooling (—), heating grower (—), cooling grower (—), and mean outside temperature (—).

One year optimization with standard settings

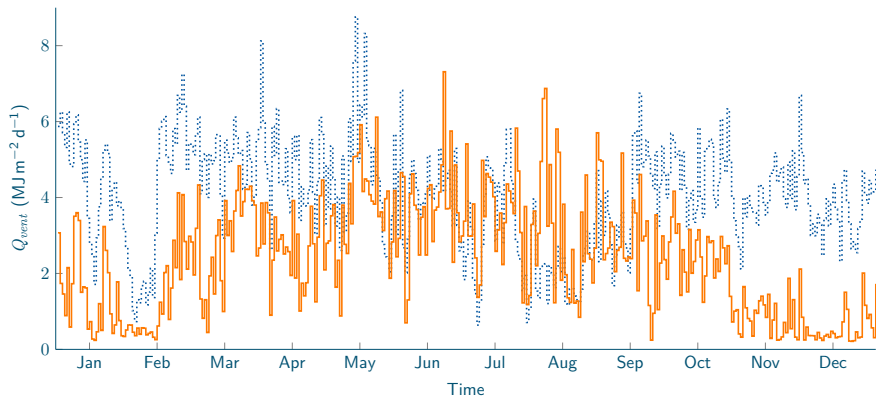


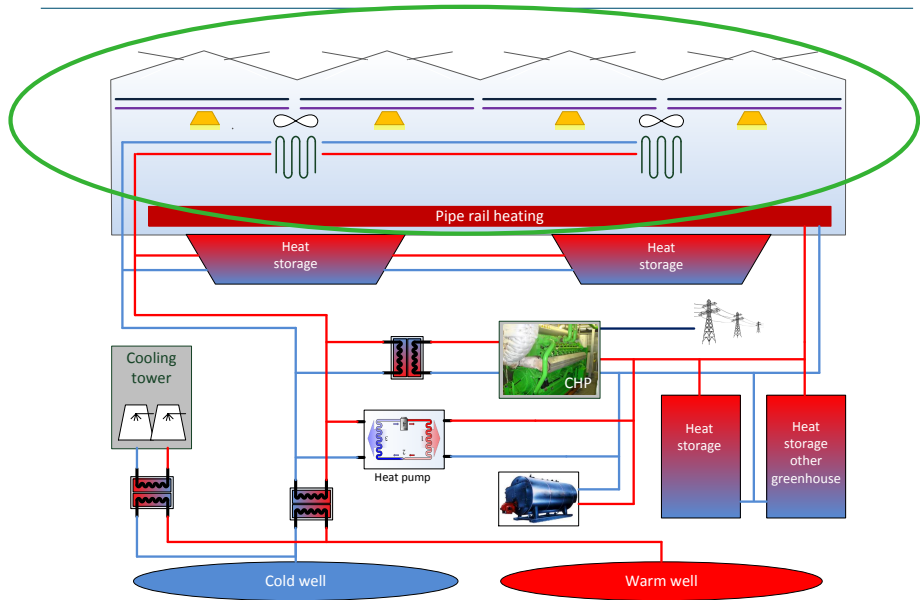
Figure : Optimal ventilation (—) and ventilation grower (—) Q_{vent} ($\text{MJ m}^{-2} \text{d}^{-1}$) for 2012.

One year optimization with standard settings

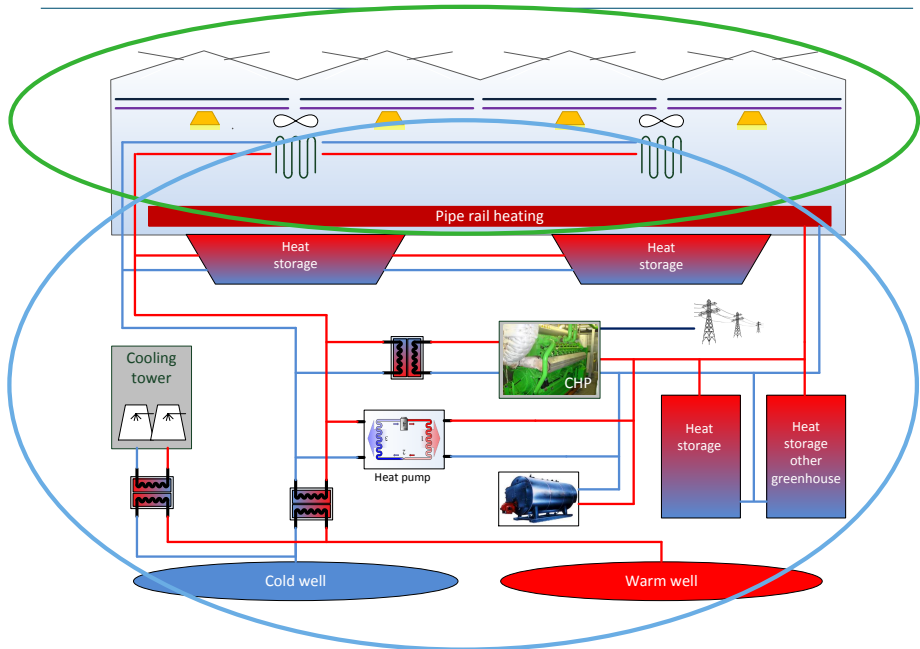
Table : Total heating, cooling, and CO₂ injection of the grower, the **optimal situation with standard settings (ss)**, and the **optimal situation with minimum pipe temperature (mp)** as used by the grower for 2012.

| | Grower | Optimal ss | Optimal mp | Unit |
|---------------------------|--------|------------|------------|------------------------------------|
| Heating | 2.08 | 1.10 | 1.49 | GJ m ⁻² y ⁻¹ |
| Cooling | 0.71 | 0.60 | 0.71 | GJ m ⁻² y ⁻¹ |
| CO ₂ injection | 95.4 | 85.7 | 85.9 | kg m ⁻² y ⁻¹ |

Stage 2: Optimization of equipment



Stage 2: Optimization of equipment



Thanks for your attention



References

- Van Beveren, P.J.M., Bontsema, J., Van Straten, G., and Van Henten, E.J. (2013). Minimal Heating and Cooling in a Modern Rose Greenhouse. In 4th IFAC Conference on Modelling and Control in Agriculture (pp. 282-287).
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